

分光计测折射率问题的不确定度分析

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摘要:分光计是大学物理实验中常用的一种精确测量角度的典型光学仪器,可以用于测量材料的折射率、色散率、光波波长和进行光谱观测等.在光谱学、材料特性、偏振光的研究、棱镜特性、光栅特性的研究中都有广泛的应用.本文以JJY型分光计为例,深入分析在分光计调节过程中的主要误差,研究减少测量不确定度、提高测量精度的方法.

关键词:分光计 误差 不确定度

分光计是一种能精密测量平面角的光学仪器.它可用作测量物质的许多光学特性,但任何量的测量过程中,由于仪器与实验者的影响,都会给结果带来不确定度.本文较全面地分析分光计在测量折射率时的不确定度问题.

1 不确定度的影响因素

1.1 狭缝宽度对不确定度的影响

不同缝宽对应的数据如表1~表5所示.

表1 缝宽大约为1.491 mm

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
189°22'	9°26'	242°51'	62°18'	99°24'	152°34.5'	53°10.5'
189°25'	9°28'	242°55'	62°21'	99°26.5'	152°38'	53°11.5'
189°19'	9°18'	242°48'	62°16'	99°18.5'	152°32'	53°13.5'

其中 θ_1^A 和 θ_2^A 表示左游标前后位置读数, θ_1^B 和 θ_2^B 表示右游标前后位置读数, θ_1 和 θ_2 表示合成后的左右游标读数,重复测量3次,顶角 $\alpha = 60^\circ$.

最小偏向角 $\bar{\delta}_{\min} = 53^\circ 12'$

平均值 $\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.66892$

不确定度

$$u_n = 0.00053 \times 1.66892 = 0.00088$$

折射率

$$n = 1.6689 \pm 0.0009$$

以下字母含义相同.

表2 缝宽大约为1.853 mm

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
170°55'	350°57'	217°51'	37°52'	260°56'	127°51.5'	47°35.5'
170°51'	350°52'	217°49'	37°48'	260°51.5'	127°49'	47°37'
170°58'	350°59'	217°54'	37°55'	260°58.5'	127°54.5'	47°36'

$$\alpha = 60^\circ$$

$$\bar{\delta}_{\min} = 47^\circ 36'$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.61144$$

$$u_n = 0.00046 \times 1.61144 = 0.00074$$

$$n = 1.6114 \pm 0.0007$$

表3 缝宽为 1.904 mm

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
263°43'	83°35'	316°25'	136°21'	173°39'	226°23'	53°24'
263°45'	83°37'	316°29'	136°26'	173°41'	226°28'	53°27'
263°41'	83°33'	316°22'	136°18'	173°37'	226°2'	53°23'

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.67018$$

$$u_n = 0.00054 \times 1.67018 = 0.00090$$

$$n = 1.6702 \pm 0.0009$$

表4 缝宽大约为 2.020 mm

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
237°42'	57°38'	286°7'	106°6'	147°4'	196°65'	49°25'
237°44'	57°41'	286°8'	106°8'	147°42.5'	197°20'	49°37.5'
237°47'	57°44'	286°9'	106°11'	147°45.5'	196°50.5'	49°5'

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 49^\circ 23'$$

$$u_n = 0.00277 \times 1.63056 = 0.00451$$

$$n = 1.630 \pm 0.004$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.63056$$

表5 缝宽为 2.099 mm

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
251°1'	71°3'	302°28'	122°27'	161°2'	212°27.5'	51°7.5'
251°23'	71°25'	302°14'	122°16'	161°24'	212°15'	51°31'
251°21'	71°22'	302°26'	122°25'	161°21.5'	212°25.5'	51°4'

$$\alpha = 60^\circ$$

$$n = 1.6490 \pm 0.0022$$

$$\bar{\delta}_{\min} = 51^\circ 1'$$

1.2 对于望远镜轴线及载物平台与中心转轴是否垂直所得数据的不确定度分析

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.64924$$

望远镜轴线及载物平台与中心转轴位置关系实验数据如表6~8所示。

$$u_n = 0.00137 \times 1.64924 = 0.00225$$

表6 望远镜轴线及载物平台与中心转轴垂直

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
117°49'	297°52'	168°41'	348°38'	207°50.5'	258°39.5'	51°29'
117°52'	297°54'	168°43'	348°39'	207°53'	258°41'	51°28'
117°59'	298°2'	168°31'	348°28'	208°29.5'	258°29.5'	50°40'

$$\alpha = 60^\circ$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.6494$$

$$\bar{\delta}_{\min} = 51^\circ 12'$$

$$n = 1.649 \pm 0.007$$

表7 望远镜轴线及载物平台与中心转轴不垂直情形

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
115°51'	295°56'	165°32'	345°34'	205°53.5'	255°33'	50°19.5'
115°43'	295°45'	166°15'	346°18'	205°44'	256°17'	51°12.5'
115°28'	295°31'	166°11'	346°15'	205°29.5'	256°13'	51°23.5'

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 50^\circ 45'$$

$$u_n = 0.008\ 59 \times 1.642\ 8 = 0.014\ 13$$

$$n = 1.64 \pm 0.01$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.642\ 8$$

表8 望远镜轴线及载物平台与中心转轴不垂直情形2

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
101°6'	281°11'	151°42'	331°46'	191°35.5'	241°44'	50°8.5'
100°56'	280°59'	152°6'	332°8'	190°57.5'	243°10'	52°12.5'
101°15'	281°18'	152°7'	332°9'	191°16.5'	242°8'	52°13.5'

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 51^\circ 28'$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.651\ 0$$

$$u_n = 0.015\ 76 \times 1.651\ 0 = 0.026\ 02$$

$$n = 1.65 \pm 0.03$$

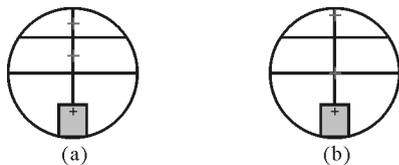


图1 十字叉丝的位置

望远镜轴线及载物平台与中心转轴不垂直的两种情况如图1(a)、(b)所示,两图分别对应表7及表8数据。

1.3 对于不同分光计两个游标不同的对称性所得数据的不确定度分析

不同分光计两个游标不同的对称性所得实验数据如表9~表11所示。

表9 对称性相差 3.08'

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
115°51'	295°56'	165°32'	345°34'	205°53.5'	255°33'	50°29.5'
115°43'	295°45'	166°15'	346°18'	205°44'	256°17'	51°22.5'
115°28'	295°31'	166°11'	346°15'	205°29.5'	256°13'	51°13.5'

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 50^\circ 45'$$

$$u_n = 0.008\ 59 \times 1.642\ 8 = 0.014\ 13$$

$$n = 1.64 \pm 0.01$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.642\ 8$$

表10 对称性相差 2.67'

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
19°38'	199°41'	68°54'	248°56'	109°39.5'	158°55'	49°15.5'
18°57'	199°	68°53'	248°56'	109°18.5'	158°55'	50°16'
52°49'	232°51'	102°11'	282°14'	142°5'	192°12.5'	50°2.5'

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 49^\circ 51'$$

$$u_n = 0.00488 \times 1.6334 = 0.00797$$

$$n = 1.633 \pm 0.008$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.6334$$

表 11 对称性相差 $10.1'$

θ_1^A	θ_1^B	θ_2^A	θ_2^B	$\theta_1 = \frac{\theta_1^A + \theta_1^B}{2}$	$\theta_2 = \frac{\theta_2^A + \theta_2^B}{2}$	$\delta_{\min} = \theta_1 - \theta_2 $
$26^\circ 31'$	$206^\circ 41'$	$77^\circ 42'$	$257^\circ 52'$	$116^\circ 36'$	$167^\circ 47'$	$51^\circ 11'$
$36^\circ 21'$	$216^\circ 32'$	$87^\circ 12'$	$267^\circ 22'$	$126^\circ 26.5'$	$177^\circ 17'$	$51^\circ 30.5'$
$55^\circ 58'$	$236^\circ 8'$	$106^\circ 49'$	$286^\circ 59'$	$146^\circ 19'$	$196^\circ 54'$	$50^\circ 35'$

$$\alpha = 60^\circ \quad \bar{\delta}_{\min} = 51^\circ 18'$$

$$\bar{n} = \sin \frac{\bar{\delta}_{\min} + \alpha}{2} \left(\sin \frac{\alpha}{2} \right)^{-1} = 1.6500$$

$$u_n = 0.00584 \times 1.6500 = 0.00963$$

$$n = 1.65 \pm 0.01$$

会有较大的误差,载物台越倾斜,误差越大且不确定度也越大,所以在分光计的调节中一定要保证望远镜轴线及载物平台与中心转轴垂直,这是实验成功的关键。

(3) 对于不同分光计两个游标不同的对称性所得数据的不确定度分析:如果对称性越差所得的实验数据的不确定度也越大。我们可以看到对称性好实验测得数据的不确定度也较小,这是因为分光计采用两个游标一起读数,然后取平均值,这样可以减小因为游标不完全对称而引起的不确定度。

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Analysis on Uncertainty of Refractivity Measurement Using Spectrometer

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Abstract: Spectrometer is a frequently-used instrument which can measure angle precisely in university physical experiments. Can be used to measure the refractive index, dispersion rate, wavelength, for spectral observations and so on. It has a wide range of applications in spectroscopy, material properties, polarized light study, prism characteristics, characteristics of the grating. With the example of JJY-Type, In-depth analysis of the adjustment process in the spectrometer's principal error of measurement. improve the precision of measurement.

Key words: spectrometer; error; uncertainty